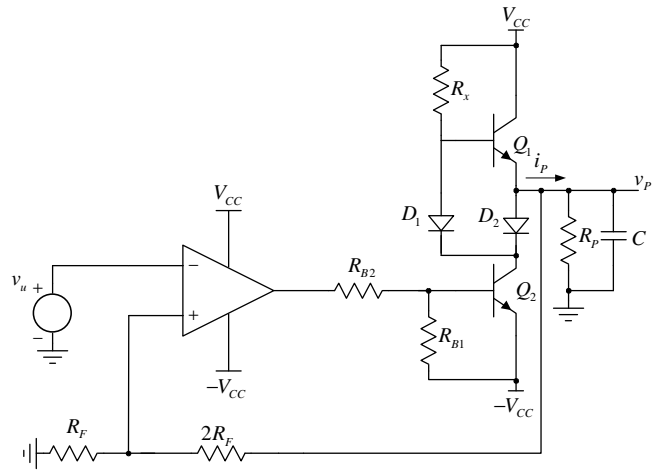


Zadatak. U kolu sa slike operacioni pojačavač se može smatrati idealnim, sa maksimalnom strujom $i_{OPmax} = 4\text{mA}$. Parametri tranzistora u kolu sa slike su $\beta_F = 100$, $V_{BE} = 0.7\text{V}$, $V_{CES} = 0.2\text{V}$ dok je $V_{CC} = 12\text{V}$, $R_p \rightarrow \infty$, $C = 2.5\mu\text{F}$, $R_x = 1\text{k}\Omega$, $R_{B1} = 1\text{k}\Omega$, $R_{B2} = 2\text{k}\Omega$. Napon na ulazu kola je trougaonog talasnog oblika periode T .

a) nacrtati i označiti dijagrame v_U , v_P , i_P , i_{C1} , i_{C2} , v_{IOP} tokom jedne periode ulaznog napona, ako je $V_u = 3\text{V}$, $T = 1\text{ms}$.



b) Pod uslovima iz tačke b) izračunati snage disipacije tranzistora Q_1 i Q_2 , i korisnu snagu koja se razvija na potrošaču.

c) Odrediti graničnu vrednost kapacitivnosti C tako da maksimalno moguća amplituda neizobličenog simetričnog napona na izlazu ne zavisi od vrednosti ove kapacitivnosti.

d) Pod uslovima iz prethodne tačke, i ako je $C = C_{gr}$ odrediti opseg mogućih vrednosti otpornosti R_{B2} tako da kolo i dalje ispravno radi

e) Ako je na ulazu kola sinusoidalni napon amplitude V_u , odrediti zavisnost srednje snage disipacije na tranzistorima Q_1 i Q_2 od V_u za $R_p = 100\Omega$, $C \rightarrow 0$, i $C \rightarrow \infty$

Rešenje:

a)

$$v_P = 3v_U = 3V_u \Delta(t)$$

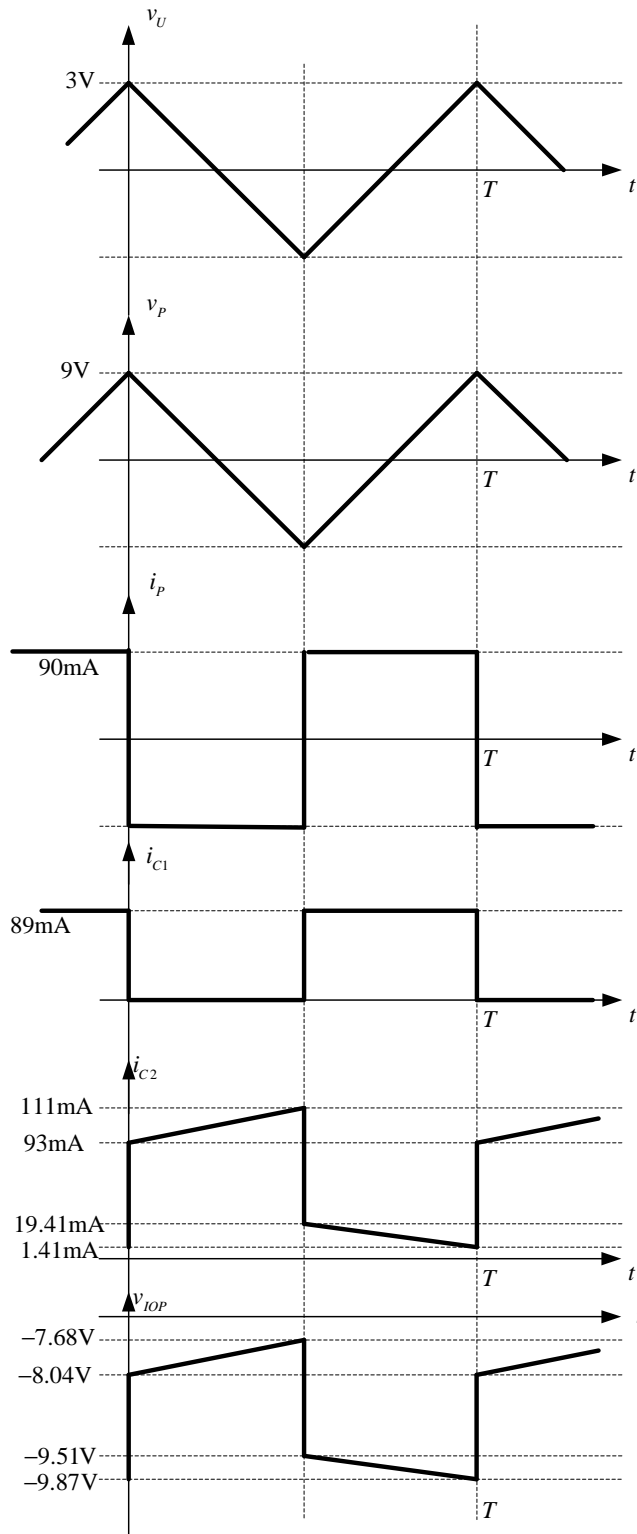
$$i_P = C \frac{dv_P}{dt} = 3CV_u \frac{d\Delta(t)}{dt} = -\frac{12CV_u}{T} \Pi(t) = -90\text{mA} \Pi(t)$$

$$i_{C1} = \begin{cases} \frac{\beta}{1+\beta} i_P, & i_P > 0 \\ 0 & i_P < 0 \end{cases} = \begin{cases} 0 & nT \leq t \leq \frac{2n+1}{2}T \\ 89\text{mA} & \frac{2n+1}{2}T \leq t \leq (n+1)T \end{cases}$$

$$i_{C2} = \begin{cases} \frac{V_{CC} - v_P}{R_x} - i_P, & nT \leq t \leq \frac{2n+1}{2}T \\ \frac{V_{CC} - V_{BE}}{R_x} - \frac{v_P}{R_x} - \frac{i_P}{1+\beta}, & \frac{2n+1}{2}T \leq t \leq (n+1)T \end{cases}$$

$$i_{C2} = \begin{cases} 102\text{mA} - 9\text{mA} \Delta(t) & nT \leq t \leq \frac{2n+1}{2}T \\ 10.41\text{mA} - 9\text{mA} \Delta(t) & \frac{2n+1}{2}T \leq t \leq (n+1)T \end{cases}$$

$$v_{IOP} = -V_{CC} + V_{BE} + R_{B2} \left(\frac{V_{BE}}{R_{B1}} + \frac{i_{C2}}{\beta} \right) = \begin{cases} -7.86\text{V} - 0.18\text{V} \Delta(t) & nT \leq t \leq \frac{2n+1}{2}T \\ -9.69\text{V} - 0.18\text{V} \Delta(t) & \frac{2n+1}{2}T \leq t \leq (n+1)T \end{cases}$$



b)

$$P_{D1} = \frac{1}{T} \int_{\frac{T}{2}}^T 89 \text{ mA} (12 - 9\Delta(t)) V dt = \frac{1}{T} \left(1068 \text{ mW} \int_{\frac{T}{2}}^T dt - 801 \text{ mW} \int_{\frac{T}{2}}^T \Delta(t) dt \right) = \dots = 0.534 \text{ W}$$

$$\begin{aligned}
P_{D2} &= \frac{1}{T} \int_0^{\frac{T}{2}} (11.3 \text{ V} + 9 \text{ V}\Delta(t))(102 \text{ mA} - 9 \text{ mA}\Delta(t))dt + \frac{1}{T} \int_{\frac{T}{2}}^T (12 \text{ V} + 9 \text{ V}\Delta(t))(10.41 \text{ mA} - 9 \text{ mA}\Delta(t))dt = \\
&= \left(\frac{1}{T} \int_0^{\frac{T}{2}} 1152.6 \text{ mW}dt - \frac{1}{T} \int_0^{\frac{T}{2}} 101.7 \text{ mW}\Delta(t)dt + \frac{1}{T} \int_0^{\frac{T}{2}} (918 \text{ mW}\Delta(t))dt - \frac{1}{T} \int_0^{\frac{T}{2}} 81 \text{ mW}\Delta^2(t)dt \right) + \\
&+ \left(\frac{1}{T} \int_{\frac{T}{2}}^T 124.92 \text{ mW}dt - \frac{1}{T} \int_{\frac{T}{2}}^T 10812 \text{ mW}\Delta(t)dt + \frac{1}{T} \int_{\frac{T}{2}}^T 93.69 \text{ mW}\Delta(t)dt - \frac{1}{T} \int_{\frac{T}{2}}^T 81 \text{ mW}\Delta^2(t)dt \right) = \\
&= 0.61 \text{ W}
\end{aligned}$$

$$P_{OUT} = 0$$

c)

Strujno ograničenje tranzistora Q_1 , kada sva struja iz otpornika R_x ode u bazu tranzistora Q_1 :

$$\begin{aligned}
V_{CC} &= \frac{R_x I_p}{1 + \beta} + V_{BE} + v_{P\max} \\
V_{CC} &= \frac{R_x}{1 + \beta} \frac{4C}{T} v_{P\max} + V_{BE} + v_{P\max} \\
v_{P\max} &= \frac{V_{CC} - V_{BE}}{1 + \frac{R_x}{1 + \beta} \frac{4C}{T}}
\end{aligned}$$

Strujno ograničenje operacionog pojačavača:

$$i_{OP} = \frac{V_{BE}}{R_{B1}} + \frac{i_{C2}}{\beta} \leq i_{OP\max}$$

Kritično je kada je struja kolektora Q_2 veća, a to je prva poluperioda

$$\begin{aligned}
i_{P\min} &= - \left(\beta \left(i_{OP\max} - \frac{V_{BE}}{R_{B1}} \right) - \frac{V_{CC} - v_{P\min1}}{R_x} \right) \\
\frac{4C v_{P\min1}}{T} &= - \left(\beta \left(i_{OP\max} - \frac{V_{BE}}{R_{B1}} \right) - \frac{V_{CC} - v_{P\min1}}{R_x} \right) = - \beta \left(i_{OP\max} - \frac{V_{BE}}{R_{B1}} \right) + \frac{V_{CC}}{R_x} - \frac{v_{P\min1}}{R_x} \\
v_{P\min1} &= - \frac{\beta \left(i_{OP\max} - \frac{V_{BE}}{R_{B1}} \right) - \frac{V_{CC}}{R_x}}{\frac{4C}{T} + \frac{1}{R_x}}
\end{aligned}$$

Naponsko zasićenje operacionog pojačavača:

$$-V_{CC} \leq -V_{CC} + V_{BE} + R_{B2} \left(\frac{V_{BE}}{R_{B1}} + \frac{i_{C2}}{\beta} \right) \leq V_{CC}$$

Negativno zasićenje se nikada neće dostići. Preostaje pozitivno:

$$-V_{CC} + V_{BE} + R_{B2} \left(\frac{V_{BE}}{R_{B1}} + \frac{i_{C2}}{\beta} \right) \leq V_{CC}$$

$$i_{C2} \leq \beta \left(\frac{2V_{CC}}{R_{B2}} - V_{BE} \left(\frac{1}{R_{B1}} + \frac{1}{R_{B2}} \right) \right)$$

$$\frac{V_{CC} - v_{P\min3}}{R_x} - \beta \left(\frac{2V_{CC}}{R_{B2}} - V_{BE} \left(\frac{1}{R_{B1}} + \frac{1}{R_{B2}} \right) \right) \leq \frac{4Cv_{P\min3}}{T}$$

$$v_{P\min3} = \frac{\frac{V_{CC}}{R_x} - \beta \left(\frac{2V_{CC}}{R_{B2}} - V_{BE} \left(\frac{1}{R_{B1}} + \frac{1}{R_{B2}} \right) \right)}{\frac{1}{R_x} + \frac{4C}{T}}$$

Naponska ograničenja:

$$v_{P\max2} = V_{CC} - V_{CES} = 11.8V$$

$$v_{P\min2} = -V_{CC} + V_{CES} + V_D = -11.1V$$

Treba da strožiji od naponskih uslova bude strožiji od strožijeg strujnog uslova:

$$|v_{P\min2}| \leq v_{P\max1}$$

$$C \leq \frac{(1+\beta)T}{4R_x} \left(\frac{V_{CC} - V_{BE}}{|v_{P\min2}|} - 1 \right) = 455nF$$

$$|v_{P\min2}| \leq |v_{P\min1}|$$

$$C \leq \frac{T}{4} \left(\frac{\beta \left(i_{OP\max} - \frac{V_{BE}}{R_{B1}} \right) - \frac{V_{CC}}{R_x}}{|v_{P\min2}|} - \frac{1}{R_x} \right) = 6.91\mu F$$

$$|v_{P\min2}| \leq |v_{P\min3}|$$

$$C \leq \frac{T}{4} \left(\frac{\beta \left(\frac{2V_{CC}}{R_{B2}} - V_{BE} \left(\frac{1}{R_{B1}} + \frac{1}{R_{B2}} \right) \right) - \frac{V_{CC}}{R_x}}{|v_{P\min2}|} - \frac{1}{R_x} \right) = 24.1mH$$

d)

$$v_{IOP} = -V_{CC} + V_{BE} + R_{B2} \left(\frac{V_{BE}}{R_{B1}} + \frac{i_{C2}}{\beta} \right)$$

$$v_{IOP\max} = -V_{CC} + V_{BE} + R_{B2} \left(\frac{V_{BE}}{R_{B1}} + \frac{i_{C2\max}}{\beta} \right) \leq V_{CC}$$

$$i_{C2\max} = \frac{V_{CC} - v_{P\min}}{R_x} - i_{P\min} = \frac{V_{CC} - v_{P\min}}{R_x} - \frac{4Cv_{P\min}}{T} = \left\langle \begin{array}{l} v_{P\min} = -11.1V \\ C = 454nF \end{array} \right\rangle = 43mA$$

$$R_{B2} \leq \frac{2V_{CC} - V_{BE}}{\frac{V_{BE}}{R_{B1}} + \frac{i_{C2\max}}{\beta}} = 20.62k\Omega$$

e)

$C \rightarrow 0$ je ekvivalentno kao da je otpornik sam

$$v_p = 3v_u = 3V_u \sin \omega t$$

$$i_p = \frac{3V_u}{R_p} \sin \omega t$$

$$i_{c1} = \begin{cases} \frac{\beta}{1+\beta} \frac{3V_u}{R_p} \sin \omega t, & i_p > 0 \\ 0 & i_p < 0 \end{cases}$$

$$i_{c2} = \begin{cases} \frac{V_{CC} - V_{BE}}{R_x} - \frac{3V_u}{R_x} \sin \omega t - \frac{1}{1+\beta} \frac{3V_u}{R_p} \sin \omega t, & i_p > 0 \\ \frac{V_{CC} - 3V_u \sin \omega t}{R_x} - \frac{3V_u}{R_p} \sin \omega t & i_p < 0 \end{cases}$$

$$P_{D1} = \frac{1}{T} \int_0^{\frac{T}{2}} \frac{V_p}{R_p} \sin \omega t (V_{CC} - V_p \sin \omega t) dt = \frac{V_{CC} V_p}{R_p} \frac{1}{T} \int_0^{\frac{T}{2}} \sin \omega t dt - \frac{V_p^2}{R_p} \frac{1}{T} \int_0^{\frac{T}{2}} \sin^2 \omega t dt =$$

$$= \frac{V_{CC} V_p}{R_p} \frac{1}{\pi} - \frac{V_p^2}{R_p} \frac{1}{4} = \frac{3V_{CC} V_u}{\pi R_p} - \frac{(3V_u)^2}{4R_p} = 0.115V_u - 0.022V_u^2$$

$$P_{D2} = \frac{1}{T} \int_0^{\frac{T}{2}} \left(\frac{V_{CC} - V_{BE}}{R_x} - \frac{V_p}{R_x} \sin \omega t - \frac{1}{1+\beta} \frac{V_p}{R_p} \sin \omega t \right) (V_p \sin \omega t + V_{CC}) dt$$

$$+ \frac{1}{T} \int_{\frac{T}{2}}^T \left(\frac{V_{CC} - V_p \sin \omega t}{R_x} - \frac{V_p}{R_p} \sin \omega t \right) (V_p \sin \omega t + V_{CC} - V_D) dt$$

$$P_{D2} = \frac{1}{T} \int_0^{\frac{T}{2}} \left(\frac{V_{CC} - V_{BE}}{R_x} V_p \sin \omega t - V_p \left(\frac{V_p}{R_x} + \frac{1}{1+\beta} \frac{V_p}{R_p} \right) \sin^2 \omega t \right) dt$$

$$+ \frac{1}{T} \int_0^{\frac{T}{2}} \left(V_{CC} \frac{V_{CC} - V_{BE}}{R_x} - V_{CC} \left(\frac{V_p}{R_x} + \frac{1}{1+\beta} \frac{V_p}{R_p} \right) \sin \omega t \right) dt$$

$$+ \frac{1}{T} \int_{\frac{T}{2}}^T \left(\frac{V_{CC} V_p \sin \omega t}{R_x} - \left(\frac{V_p^2}{R_x} + \frac{V_p^2}{R_p} \right) \sin^2 \omega t \right) dt$$

$$+ \frac{1}{T} \int_{\frac{T}{2}}^T \left(\frac{V_{CC} (V_{CC} - V_D)}{R_x} - (V_{CC} - V_D) \left(\frac{V_p}{R_x} + \frac{V_p}{R_p} \right) \sin \omega t \right) dt$$

$$\begin{aligned}
P_{D2} &= \left(V_{CC} \frac{V_{CC} - V_{BE}}{R_x} \right) \frac{1}{T} \int_0^{\frac{T}{2}} dt + \left(\frac{V_{CC} - V_{BE}}{R_x} V_p - V_{CC} \left(\frac{V_p}{R_x} + \frac{1}{1 + \beta} \frac{V_p}{R_p} \right) \right) \frac{1}{T} \int_0^{\frac{T}{2}} \sin \omega t dt - \\
&- V_p \left(\frac{V_p}{R_x} + \frac{1}{1 + \beta} \frac{V_p}{R_p} \right) \frac{1}{T} \int_0^{\frac{T}{2}} \sin^2 \omega t dt + \\
&+ \frac{V_{CC} (V_{CC} - V_D)}{R_x} \frac{1}{T} \int_{\frac{T}{2}}^T dt - \left((V_{CC} - V_D) \left(\frac{V_p}{R_x} + \frac{V_p}{R_p} \right) - \frac{V_{CC} V_p}{R_x} \right) \frac{1}{T} \int_{\frac{T}{2}}^T \sin \omega t dt - \left(\frac{V_p^2}{R_x} + \frac{V_p^2}{R_p} \right) \frac{1}{T} \int_{\frac{T}{2}}^T \sin^2 \omega t dt = \\
&= \left(V_{CC} \frac{V_{CC} - V_{BE}}{R_x} \right) \frac{1}{2} + \left(\frac{V_{CC} - V_{BE}}{R_x} V_p - V_{CC} \left(\frac{V_p}{R_x} + \frac{1}{1 + \beta} \frac{V_p}{R_p} \right) \right) \frac{1}{\pi} - V_p \left(\frac{V_p}{R_x} + \frac{1}{1 + \beta} \frac{V_p}{R_p} \right) \frac{1}{4} + \\
&+ \frac{V_{CC} (V_{CC} - V_D)}{R_x} \frac{1}{2} + \left((V_{CC} - V_D) \left(\frac{V_p}{R_x} + \frac{V_p}{R_p} \right) - \frac{V_{CC} V_p}{R_x} \right) \frac{1}{\pi} - \left(\frac{V_p^2}{R_x} + \frac{V_p^2}{R_p} \right) \frac{1}{4}
\end{aligned}$$

$$P_{D2} = -\frac{V_p^2}{4} \left(\frac{2}{R_x} + \frac{\beta + 2}{\beta + 1} \frac{1}{R_p} \right) - \frac{V_p}{\pi} \left(V_{BE} \left(\frac{1}{R_p} + \frac{2}{R_x} \right) - \frac{\beta}{1 + \beta} \frac{V_{CC}}{R_p} \right) + \frac{V_{CC} (V_{CC} - V_D)}{R_x}$$

$$P_{D2} = -0.027V_u^2 + 0.105V_u + 0.136$$

$C \rightarrow \infty$ je ekvivalentno kao da je otpornik u kratkom spoju, negativna povratna sprega je raskinuta, operacioni pojačavač će biti u naponskom zasićenju.

Kada je $v_u > 0$ operacioni pojačavač je u negativnom zasićenju i tranzistor Q_2 je isključen

$$\begin{aligned}
P_{D2} &= 0 \\
\text{Važi } i_{C1} &= \beta \frac{V_{CC} - V_{BE}}{R_x} = 1.13A \\
P_{D1} &= V_{CC} i_{C1} = 13.56W
\end{aligned}$$

Kada je $v_u < 0$ operacioni pojačavač je u pozitivnom zasićenju i tranzistor Q_2 je uključen.

Tranzistor Q_1 je isključen jer je $v_{BE1} = (v_p - V_D + V_D) - v_p = 0$.

$$\begin{aligned}
i_{B2} &= \frac{2V_{CC} - V_{BE}}{R_{B2}} - \frac{V_{BE}}{R_{B1}} = 10.95mA \\
i_{C2} &= \beta i_{B2} = 1.095A \\
P_{D2} &= (-V_D + V_{CC}) i_{C2} = 12.3735W \\
P_{D1} &= 0 \\
P_{D1} &= \frac{13.56 + 0}{2} = 6.78W \\
P_{D2} &= \frac{12.3735}{2} = 6.18675W
\end{aligned}$$